

**GANE-1
GANE-1A**

**Conventional Core Analysis on GANE-1
and GANE-1A cores, Eqalulik, Nuussuaq,
West Greenland
Andersen, G.**

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Eqalulik, Nuussuaq, West Greenland

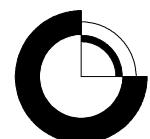
Gert Andersen



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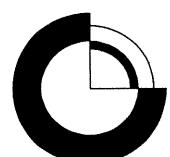
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Conventional core analysis on GANE#I and GANE#IA cores

Eqalulik, Nuussuaq, West Greenland

By Gert Andersen



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1. Introduction

In May 1995 grønArctic Energy Inc., Canada was awarded an exclusive licence to explore for hydrocarbons on the southern and western part of the Nuussuaq peninsula, West Greenland. As part of the commitments under this licence three slim core holes GANE#1, GANK#1 and GANT#1 were drilled in July and August 1995.

The GANE#1 well was drilled in two sections. The upper part GANE#1 and a side-track GANE#1A below.

The Core Analysis Laboratory at The Geological Survey of Denmark and Greenland has received parts of these two cores for conventional core analysis. Table 1.1 show box numbers, depth intervals and measured core size for the analyzed cores:

Table 1.1: List of analyzed cores.

Core	Box numbers	Top	Bottom	Core size
GANE#1	156 - part of 204	487,28		ø47mm
GANE#1	Part of 204 - 205		636,86 *	ø36mm
GANE#1A	206 - 258	535,57	706,68	ø36mm

* Corrected due to error on bottom depth on box 204 and top/bottom depth on box 205.

The analysis covers the following services:

- Spectral core gamma log
- Gas permeability
- Porosity
- Grain density

2. Sampling and analytical procedures

Cores were transported from Greenland to Copenhagen in 1,2m boxes. Boxes were made of a toplayer and a bottomlayer only, fixed together without any side walls. Every box contained 3 meters (m) core interval parted in three 1 m lengths. These lengths are named A, B and C from top to bottom in this analysis programme.

The cores were restored in another set of boxes at the arrival to Denmark.

2.1 Spectral core gamma log

Spectral core gamma logs were made with a scanning speed of 1 cm per minute. The cores were scanned without the boxes.

2.2 Plugging

Following the gamma activity recording, the plugging programme was conducted. Horizontal 1" plugs were drilled for every 1m of core if possible. Standard plugging depth was 0,5m below top of section A, B and C.

Some sections were shaled and plugging was impossible in these sections. Other plugs were drilled in the other boxes, to supply the standard plugging. Depths were selected due to the visual variation in the core, giving a better representation of the variations in the core.

The missing plugs from these sections se plugs were saved for drilling supply plugs in other intervals, giving a better representation of the variation in the core.

Plug depths were calculated as distance from top of the 3m boxes. The core length expanded for some of the cores during the restoring in other boxes and during the spectral core gamma log, and the distance from top of 3m box were calculated by the following algorithm:

A sections: Measured distance from top of box

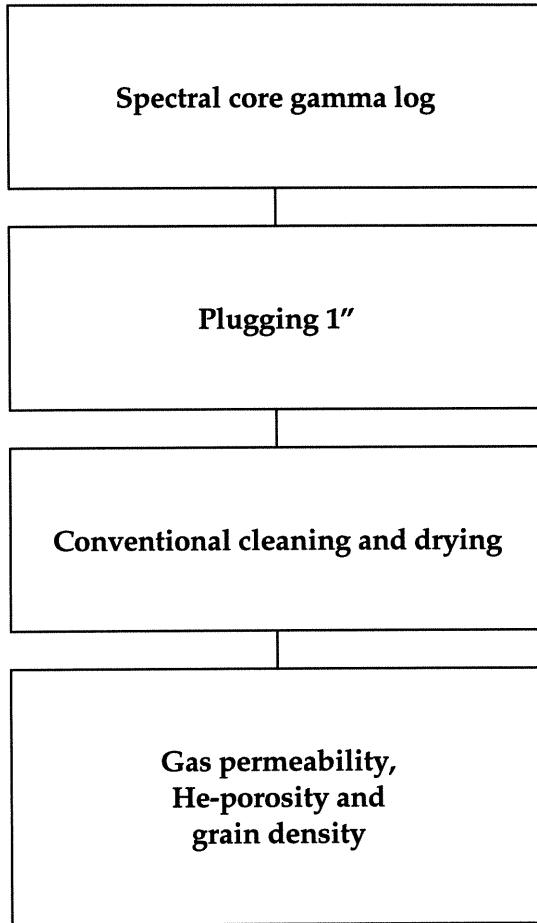
B sections: Measured distance from top of box plus measured length of A

C sections: Measured distance from top of box plus measured length of A and B

2.3 Conventional core analysis

The plugs were cleaned in Soxhlet extractors and then dried at 110°C. Conventional core analysis including He-porosity, grain density and gas permeability was performed. The permeability was measured using a sleeve pressure of 400 psi.

3. Flow diagram of the analytical procedures



4. Analytical methods

The following is a short description of the methods used by the Core Analysis Laboratory. For a more detailed description of methods, instrumentation and principles of calculation the reader is referred to API recommended practice for core analysis procedure (API RP 40, 1960).

4.1 Spectral core gamma log

The natural gamma radiation of a core is recorded within an energy window of 0.5 - 3.0 MeV, using Tl activated NaI scintillation detectors (Bicron), connected to a multichannel analyzer (Canberra).

The core is passed through a lead shielded tunnel at constant speed while the gamma activity is continuously recorded. Refer to Chapter 2 for the scanning speed used. The integrated gamma activity is recorded at regular intervals, either every 10 cm or every 3". The gamma activity represents the mean activity over a 10 cm or 3" interval, the assigned depth being the middle of the interval. The measured gamma activity is corrected for background activity, and in the case of sleeved core, also for activity of the sleeve.

Gamma activity is normally reported in counts per minute (cpm) at the actual core diameter. The following empirical relationship between "GAPI" from wireline logs and the actual cpm from GEUS core gamma logs (GEUS-cpm) has been established. The relationship should be used as a guideline only:

$$\text{GAPI} = \text{GEUS-cpm} * (10\text{cm}/d)^2 / 18,2$$

where d is core diameter in cm.

Radiation from decay of potassium and the uranium and thorium decay series are recorded in separate energy windows. Concentrations are calculated using synthetic standards of concrete doped with radioactive minerals in decay equilibrium. Concentrations of K, U and Th are reported as % K, ppm U and ppm Th, respectively. Relevant ratios are given.

4.2 Conventional cleaning and drying

The plugs are drilled and trimmed to a standard size of 1" diameter and 1.5" length. The samples are then placed in a Soxhlet extractor, which continuously soaks and washes the samples with methanol. This process removes water and dissolves salt precipitated in the pore space of the rock. Extraction is terminated when no chloride ions are present in the methanol. Samples containing hydrocarbons are then cleaned in toluene until a clear solution is obtained. Samples are vacuum dried at 90°C or 110°C, or they are humidity dried at 60°C and 40% relative humidity until constant weight occurs, depending on the requirements of the client.

4.3 Gas permeability

The plug is mounted in a Hassler core holder, and a confining pressure of 400 psi applied to the sleeve. The specific permeability to gas is measured by flowing nitrogen gas through a plug of known dimensions at differential pressures between 0 and 1 bar. No back pressure is applied. The readings of the digital gas permeameter are checked regularly by routine measurement of permeable steel reference plugs.

4.4 He-porosity and grain density

The porosity is measured on cleaned and dried samples. The porosity is determined by subtraction of the measured grain volume and the measured bulk volume. The Helium technique, employing Boyle's Law, is used for grain volume determination, applying a double chambered Helium porosimeter with digital readout, whereas bulk volume is measured by submersion of the plug in a mercury bath using Archimedes principle. Grain density is calculated from the grain volume measurement and the weight of the cleaned and dried sample.

4.5 Precision of analytical data

The Table below gives the precision (reproducibility) at the 68% level of confidence (+/- 1 standard deviation) for routine core analysis measurements performed at the GEUS Core Analysis Laboratory.

Measurement	Range, mD	Precision
Grain density		0.003 g/cc
Porosity		0.1 porosity-%
Gas Permeability	0.001-0.01 0.01-0.1 > 0.1	25% 15% 4%

The precision of the fluid saturation determination depends on the pore volume of the plug. The greater the volume of the plug and the greater the porosity of the plug, better precision is obtained. The following Table gives the precision in absolute percent-point.

Porosity	1" x 1.5" plugs	1.5" x 3" plugs
> 20%	5%	1%
10-20%	10%	2%
5-10%	20%	5%
< 5%	> 20%	> 5%

Certain factors might alter the stated precision of the fluid saturation determination. Loss of material during handling of the plug will result in an increase in the calculated oil saturation, and a similar decrease in the calculated gas saturation. This may occur for fragile or loosely consolidated rocks or if the rock contains dissolvable matter like halite. As the lost material usually has a greater density than oil, it may happen that the esti-

mated volume of oil and the measured volume of water all together take up more space than the actual pore volume after cleaning.

The precision of the total gamma activity analysis is calculated from counting statistics. The following list shows the dependency of reproducibility on count rate at 2 standard deviations.

Count rate (cpm)	Reproducibility (cpm)
125	7.1
250	10.0
500	14.2
1000	20.1
2000	28.4
4000	40.2

Reproducibility (precision) of the amount of uranium, thorium and potassium from gamma radiation is dependent on concentration. Two values for reproducibility are given, one for normal to high concentration range, and one for low concentration range. The latter also defines the detection limit (LLD). The reproducibility values are applicable to total gamma activity above and below 800 cpm, respectively.

	K(%)	U(ppm)	Th(ppm)
Reproducibility			
Normal to high range	0.07	0.60	1.14
Low range (LLD)	0.02	0.45	0.48
Accuracy	0.02	0.45	0.48

Accuracy is calculated as mean deviation from the accepted concentration of one internal standard. This value is only applicable to low concentrations. For high concentrations the high range reproducibility may serve as an approximation to accuracy. Accuracy is reported as an arithmetic mean.

5. Results

5.1 Spectral core gamma log

Spectral core gamma logs are made in the three sections, GANE1-1, GANE1-2 and GANE1A as shown in Table 5.1 below. The gamma logs are presented in the log sheet below. Please note: The logs "Total gamma (cps)" are in cps without correction for differences in core dimensions. Box numbers with ø36mm core are shown with a dotted background and box numbers with ø47mm are shown with a white background.

The spectral log is made with a measure time of 595sec at each window and a presumed core density at 2,020g/ccm.

Drillers information on top and bottom depth for box no. 204 and 205 is probably erroneous. There is a 3 m depth error, and a correction for this error gave a perfect correlation between the spectral core gamma logs for GANE#1 and GANE#1A.

Table 5.2: Depth corrections in metre for box 204 and 205.

Box	Top	Bottom	Corrected top	Corrected bottom
204	630,42	636,62		633,62
205	636,62	639,86	633,62	636,86

Core gammalog for GANE#1 and GANE#1A below:

GANE 1

Core gamma log

ø47mm/ø36mm

Depth vs.

Th/K

Th/U

U/K

Thorium

Uranium

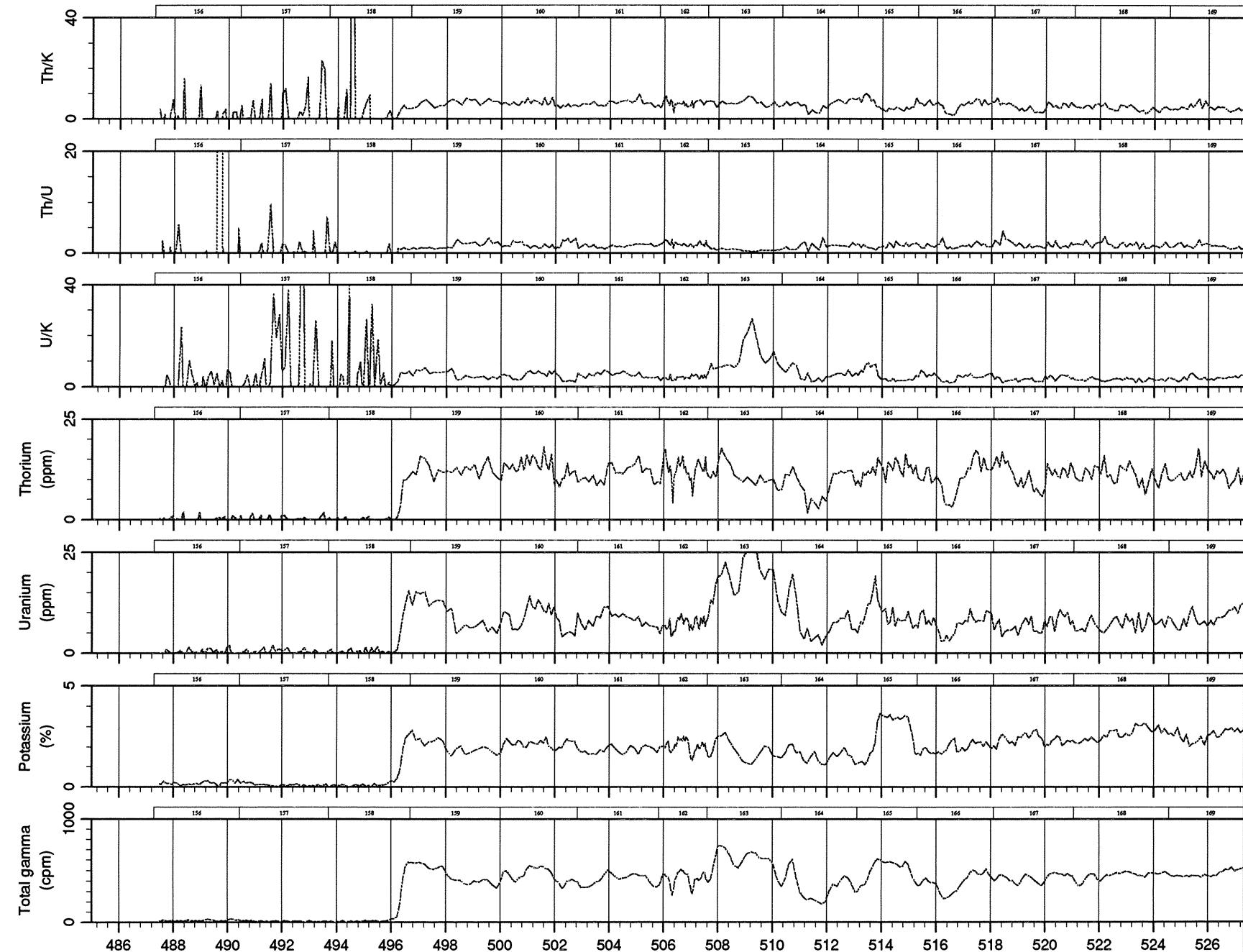
Potassium

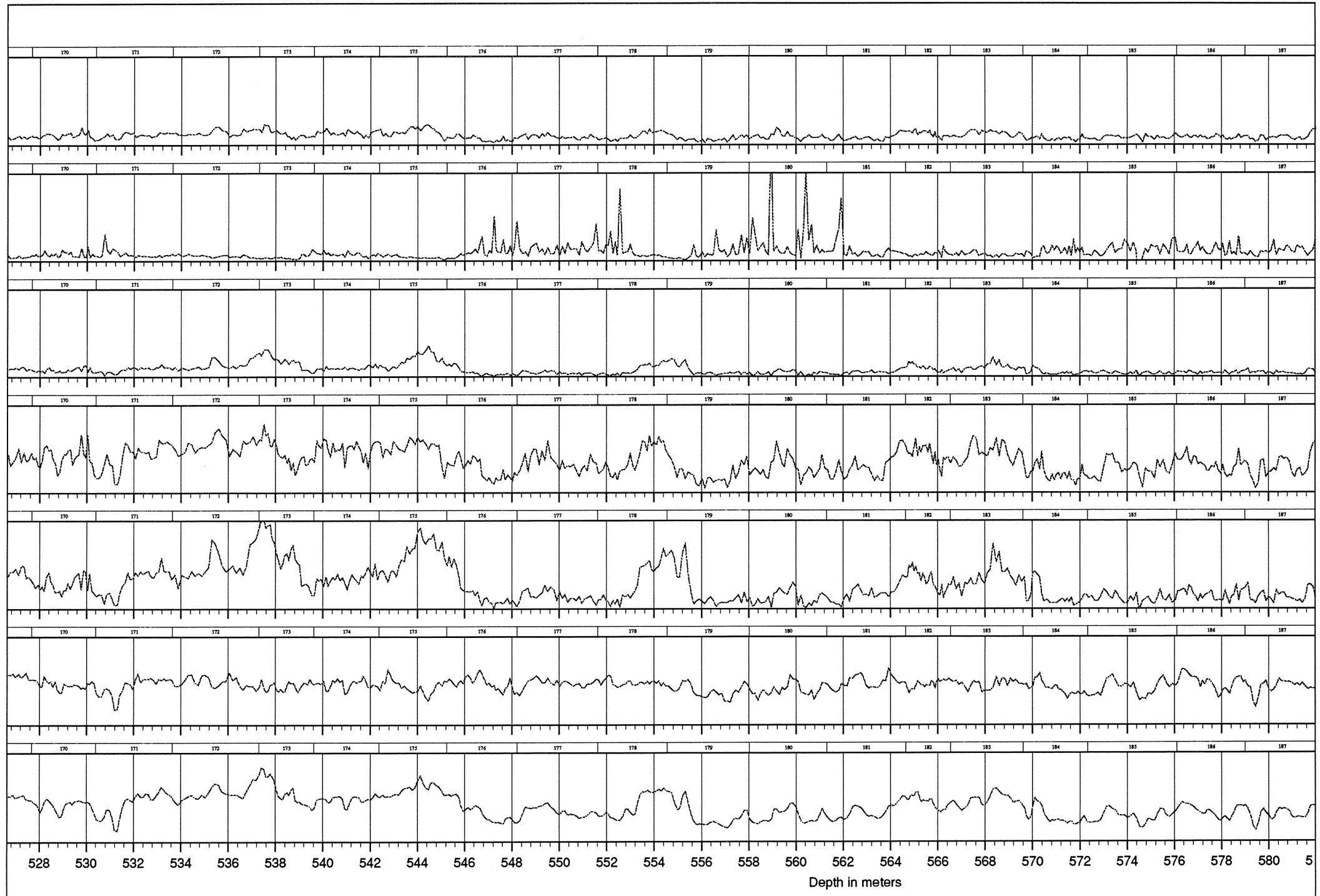
Total Gamma

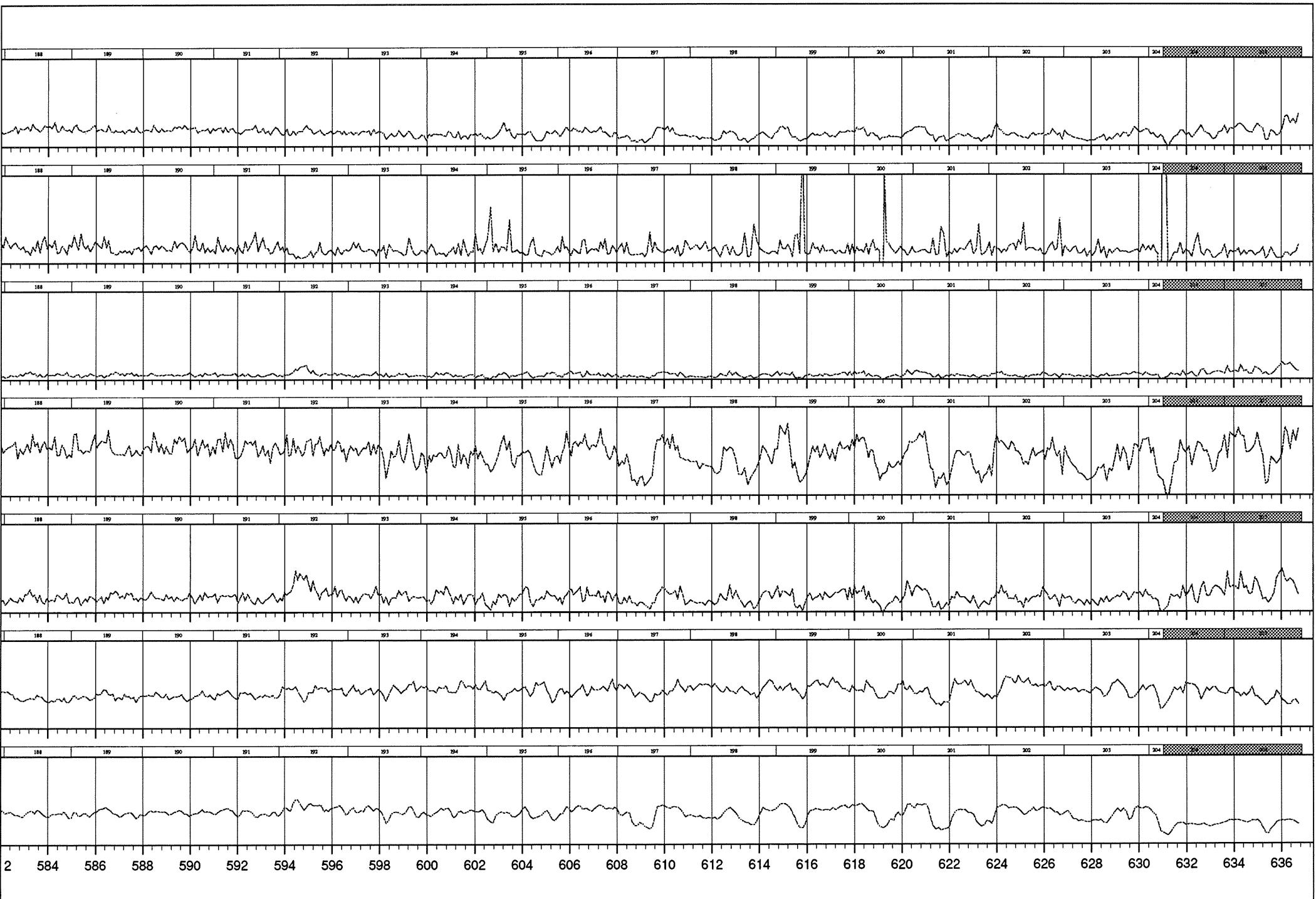
Scale 1:200

Legend

~ Gane1







GANE 1A

Core gamma log

Ø36mm core

Depth vs.

Th/K

Th/U

U/K

Thorium

Uranium

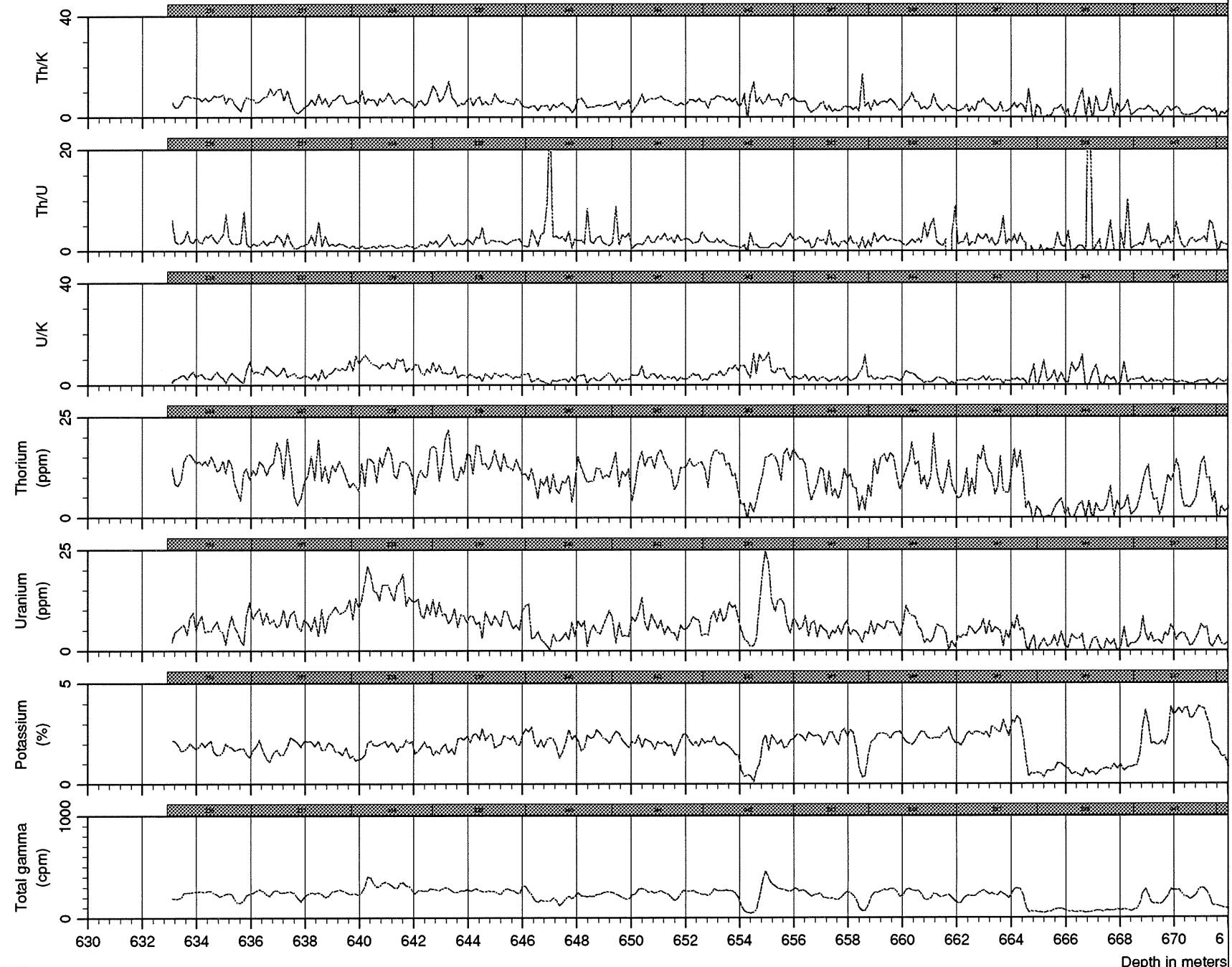
Potassium

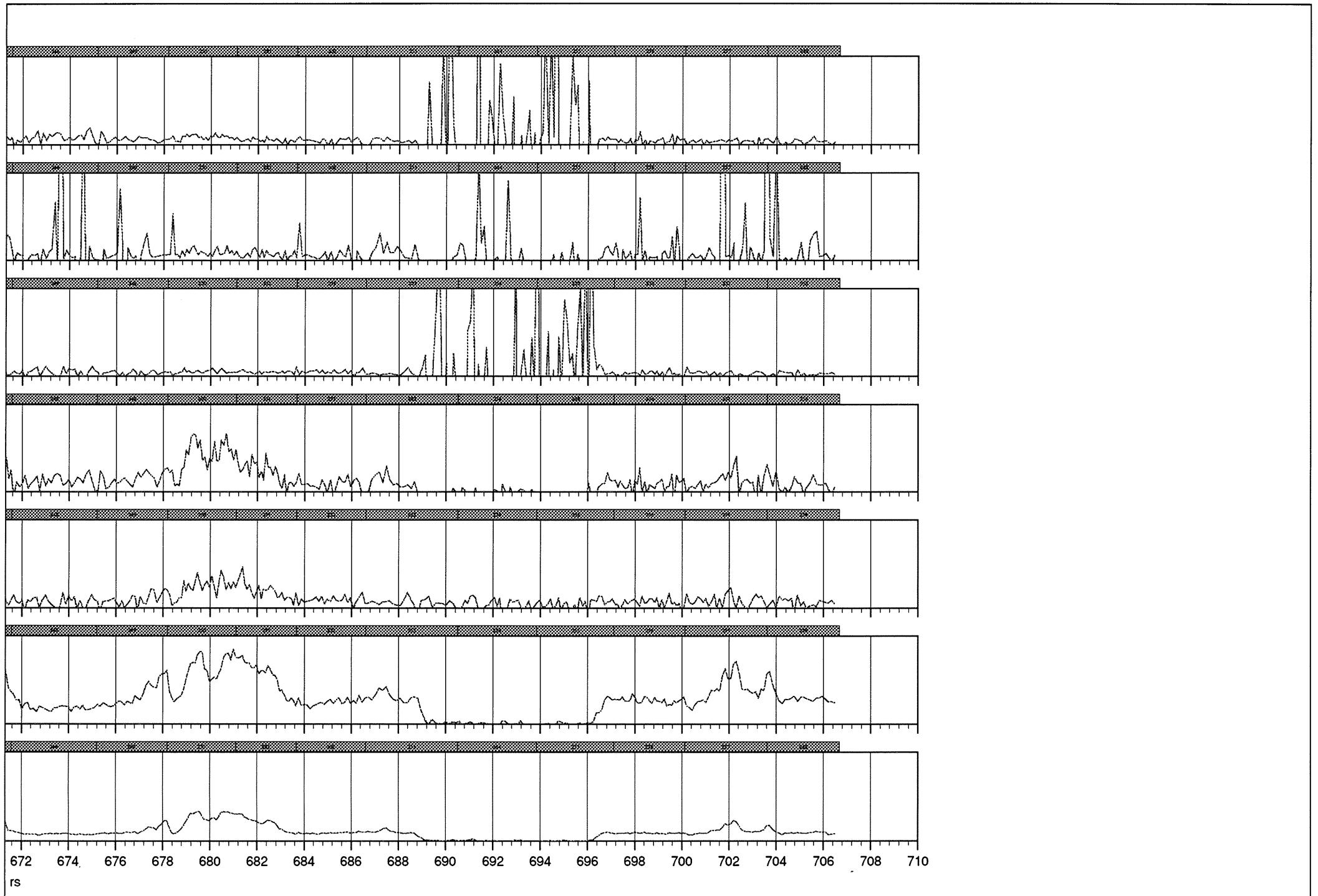
Total Gamma

Scale 1:200

Legend

~~~~ Gane 1A





## 5.2 Statistical information

Frequency plots of gas permeability, porosity and grain density and cross plots are made together with statistic information on GANE#1, GANE#1A and the total sum of GANE#1 and GANE#1A plugs.

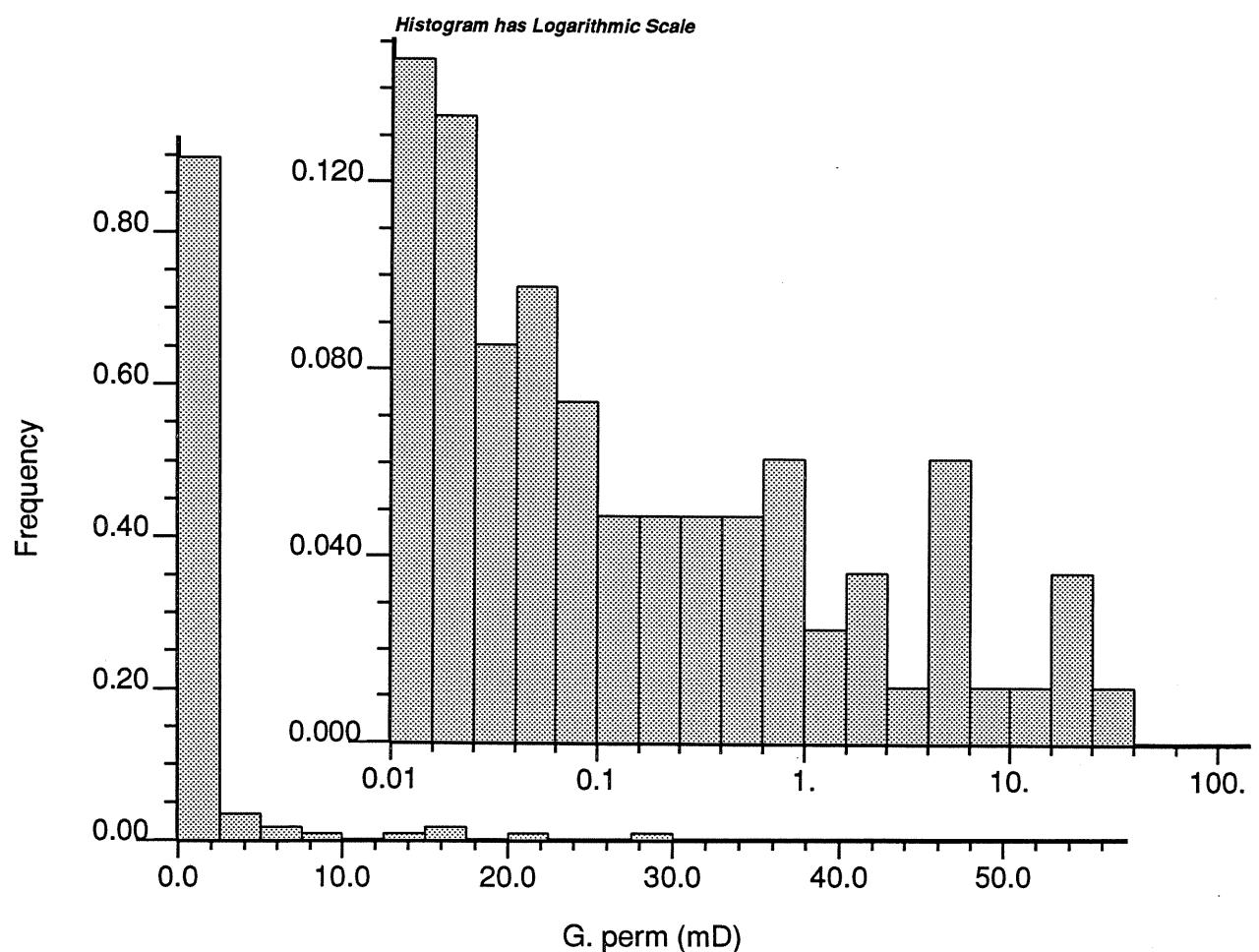
These statistical information is calculated on data only from samples with measured porosity and non-zero permeability. The numbers of these samples are shown in the Table below:

| Population         | Numbers of plug samples | Numbers of plugs samples used for statistic calculations |
|--------------------|-------------------------|----------------------------------------------------------|
| GANE#1             | 131                     | 101                                                      |
| GANE#1A            | 67                      | 53                                                       |
| GANE#1 and GANE#1A | 198                     | 154                                                      |

### 5.2.1 GANE#1, Gas permeability

Permeability:

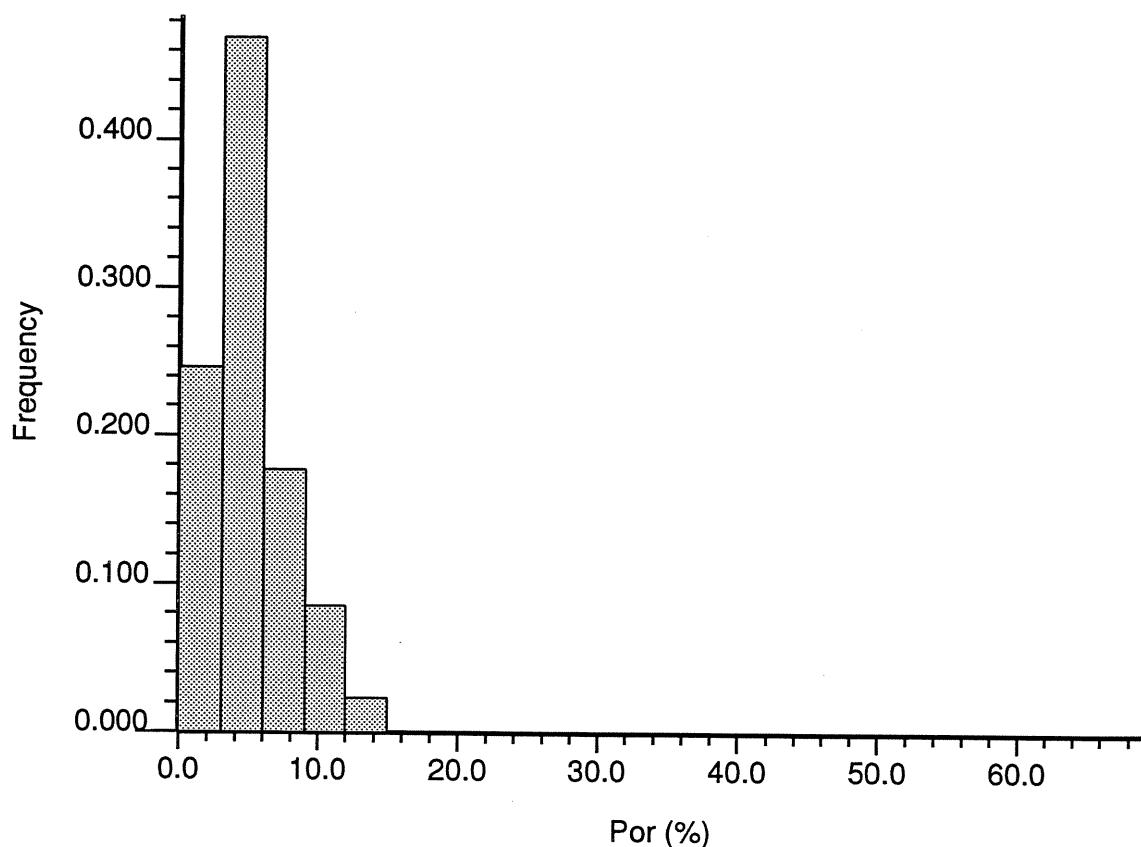
Geometric average: 0.08 mD  
 Aritmetric average: 1.51 mD  
 Harmonic average: 0.02 mD



### 5.2.2 GANE#1, Porosity

Porosity:

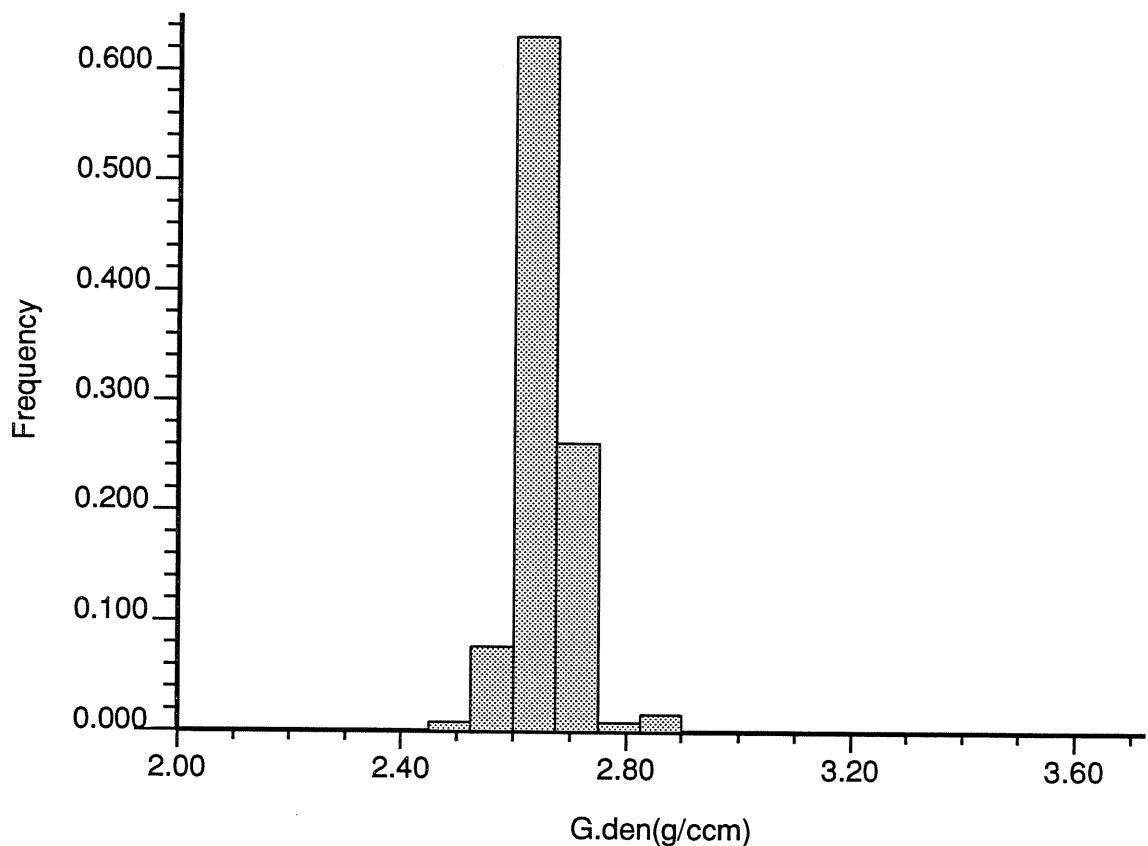
Mean porosity: 5.41 %  
Variance on porosity: 8.25 %<sup>2</sup>



### 5.2.3 GANE#1, Grain density

Grain density:

Mean grain density: 2,66 %  
Variance on mean gr. den.: 0,01 %<sup>2</sup>



### 5.2.4 GANE#1, Porosity vs. gas permeability

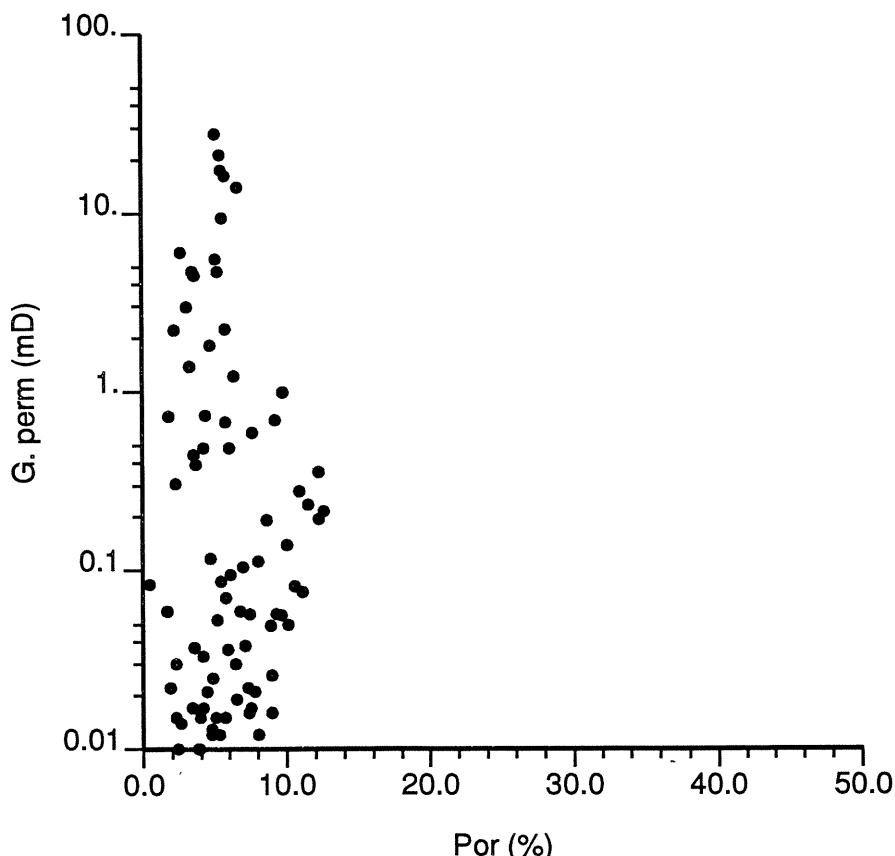
Statistics calculated from linear regression of permeability on porosity:

$$\text{Model: } \text{Log10(Permeability)} = \text{Intercept} + \text{Slope} * \text{Porosity} + \text{Residual}$$

|                                         |                   |
|-----------------------------------------|-------------------|
| Degrees of freedom:                     | 99                |
| Coefficient of determination:           | 0.041             |
| Standard error on the regression:       | 1.027 log(mD)     |
| Estimated intercept:                    | -1.486 log(mD)    |
| Estimated standard error of intercept : | 0.219 log (mD)    |
| Estimated slope:                        | 0.07383 log(mD)/% |
| Estimated standard error of slope:      | 0.03576 log(mD)/% |

Please note that the regression statistics pertain to log permeability values.

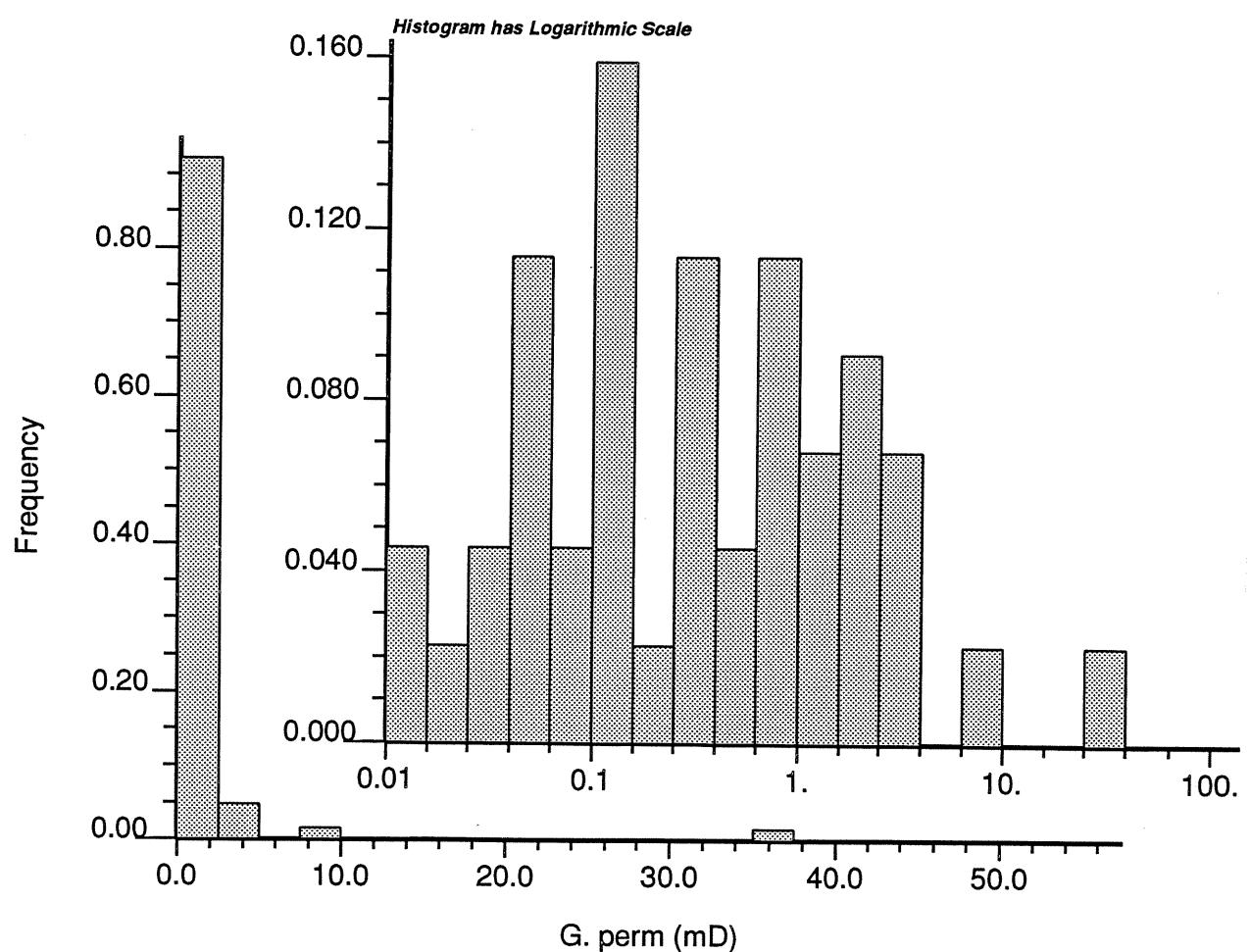
The coefficient of determination gives the fraction of the total variation squared which is explained by the mode. The standard error on the regression gives the mean 1 sigma error on the log permeability estimates.



### 5.2.5 GANE#1A, Gas permeability

Permeability:

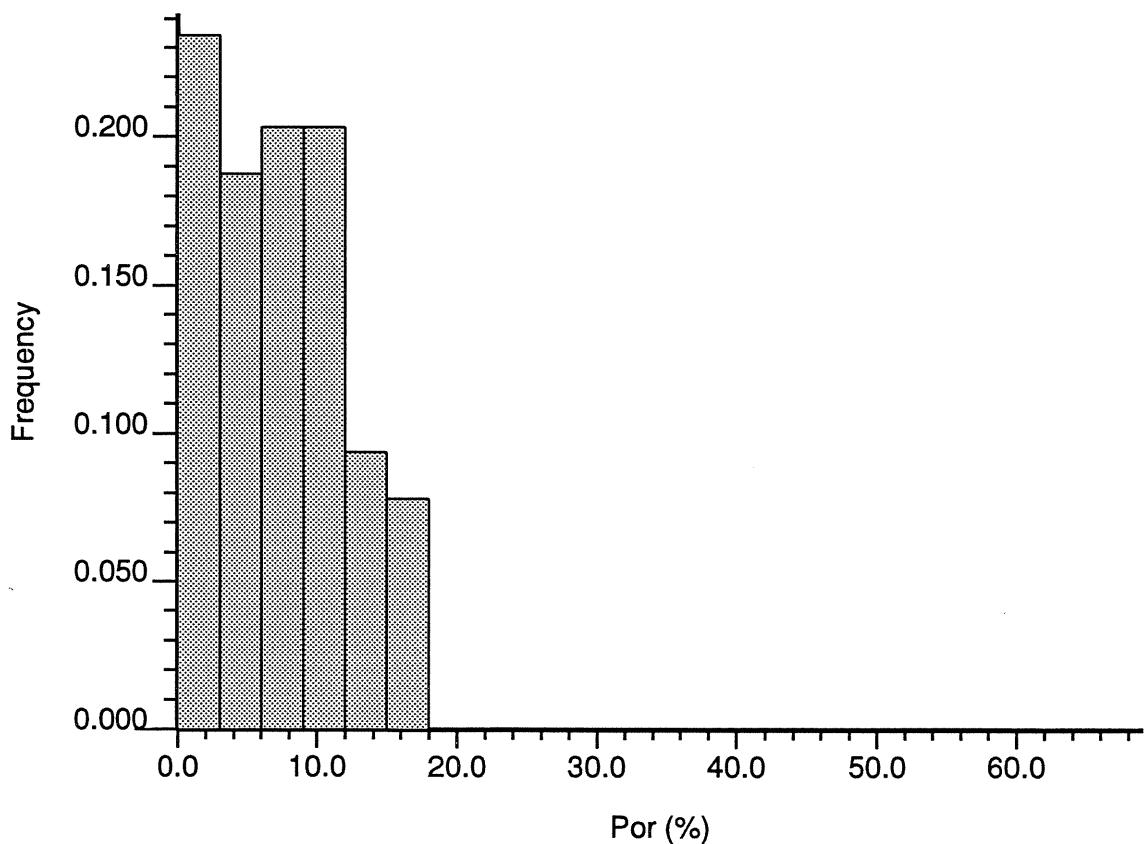
Geometric average: 0,16 mD  
 Aritmetric average: 1,36 mD  
 Harmonic average: 0,03 mD



### 5.2.6 GANE#1A, Porosity

Porosity:

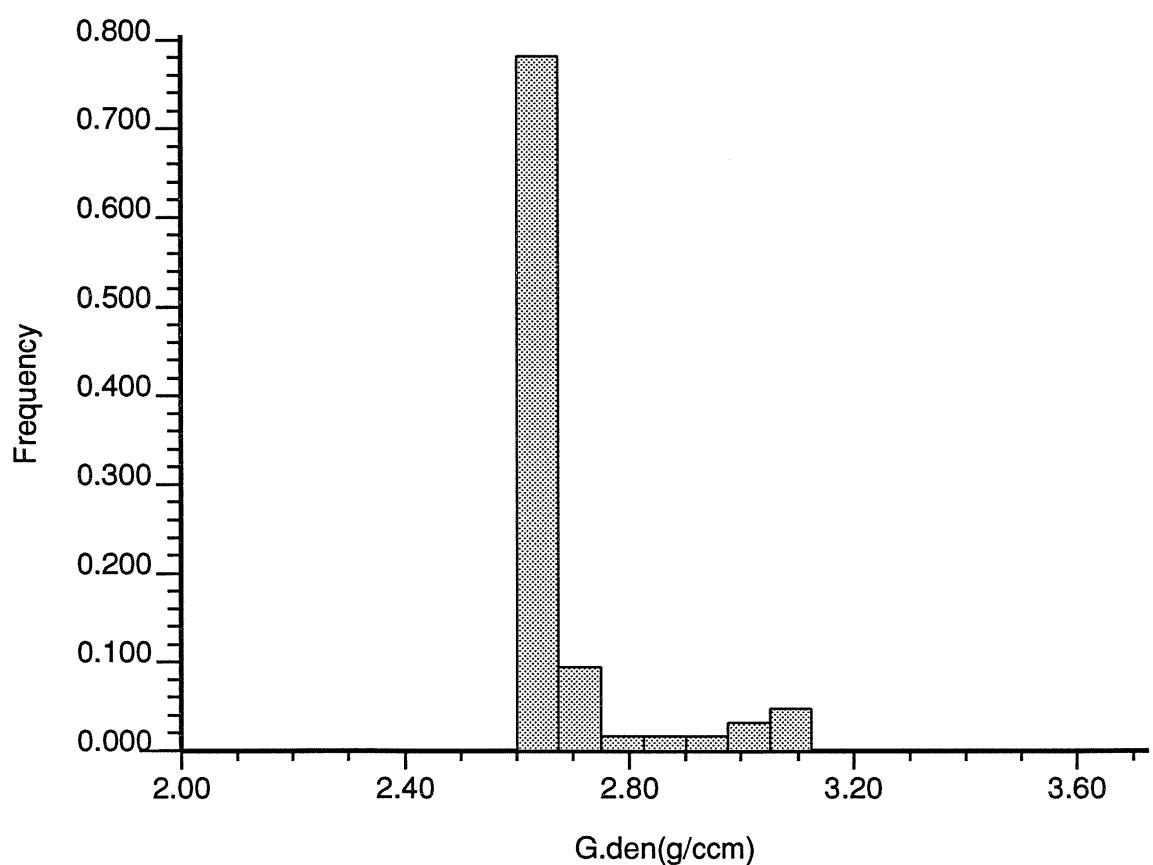
Mean porosity: 8,48 %  
Variance on porosity: 16,96 %<sup>2</sup>



### 5.2.7 GANE#1A, Gain density

Grain density:

Mean grain density: 2,69 %  
Variance on mean gr. den.: 0,01 %<sup>2</sup>



### 5.2.8 GANE#1A, Porosity vs. gas permeability

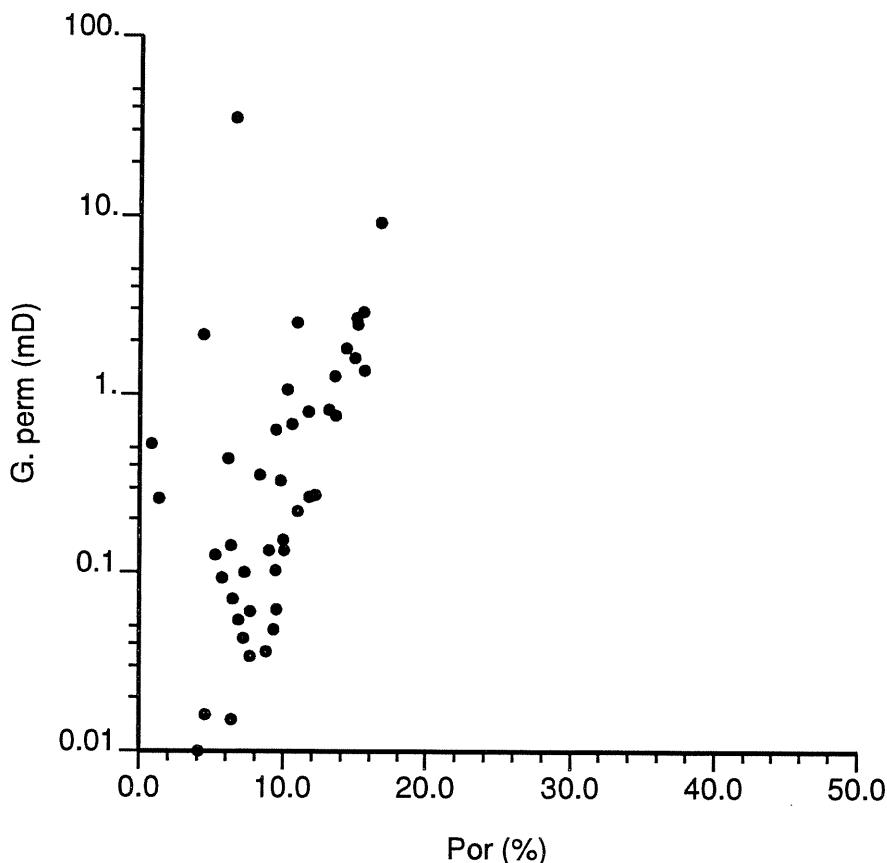
Statistics calculated from linear regression of permeability on porosity:

$$\text{Model: } \text{Log10(Permeability)} = \text{Intercept} + \text{Slope} * \text{Porosity} + \text{Residual}$$

|                                         |                     |
|-----------------------------------------|---------------------|
| Degrees of freedom:                     | 51                  |
| Coefficient of determination:           | 0,464               |
| Standard error on the regression:       | 0,707 log(mD)       |
| Estimated intercept:                    | -2,146 log(mD)      |
| Estimated standard error of intercept : | 0,224 log (mD)      |
| Estimated slope:                        | 0,15809 log(mD) / % |
| Estimated standard error of slope:      | 0,02379 log(mD) / % |

Please note that the regression statistics pertain to log permeability values.

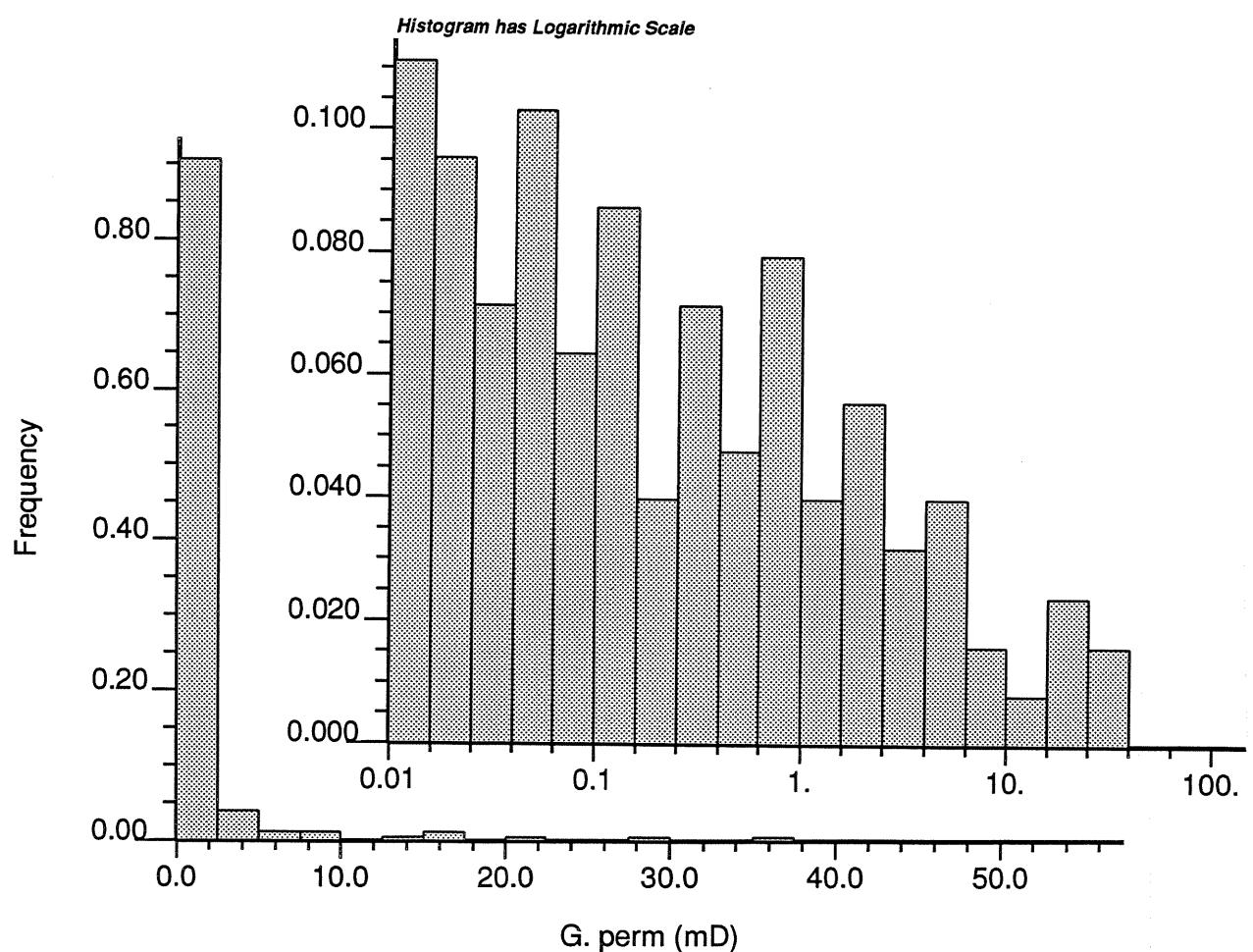
The coefficient of determination gives the fraction of the total variation squared which is explained by the mode. The standard error on the regression gives the mean 1 sigma error on the log permeability estimates.



### 5.2.9 GANE#1+1A, Gas permeability

Permeability:

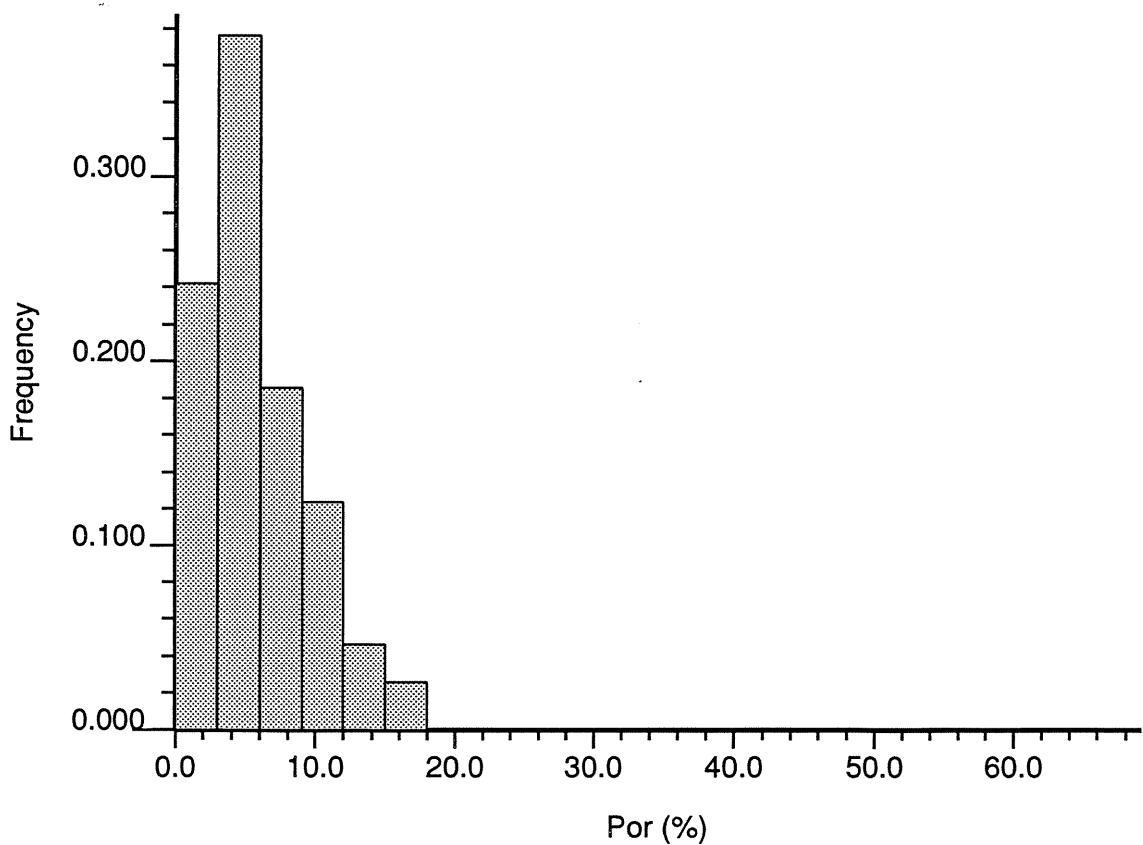
Geometric average: 0,10 mD  
 Aritmetric average: 1,46 mD  
 Harmonic average: 0,02 mD



### 5.2.10 GANE#1+1A, Porosity

Porosity:

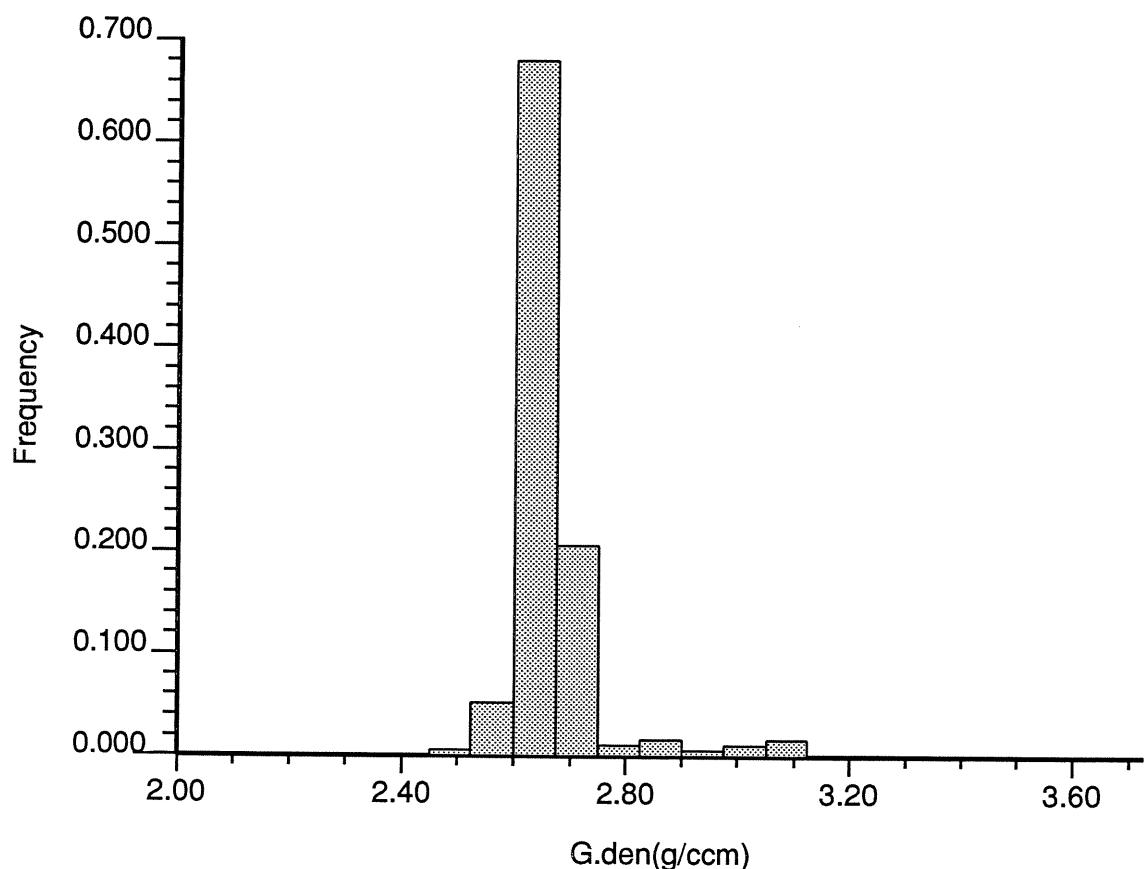
Mean porosity: 6,46 %  
Variance on porosity: 13,29 %<sup>2</sup>



### 5.2.11 GANE#1+1A, Grain density

Grain density:

Mean grain density: 2,67 %  
Variance on mean gr. den.: 0,01 %<sup>2</sup>



### 5.2.12 GANE#1+1A, Porosity vs. gas permeability

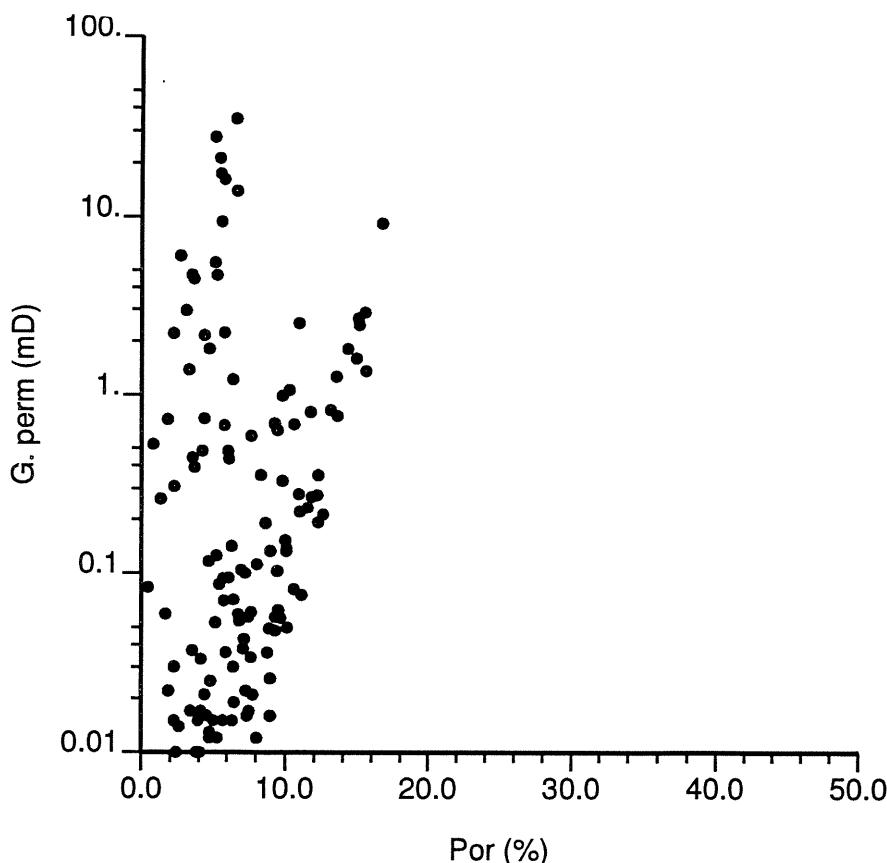
Statistics calculated from linear regression of permeability on porosity:

$$\text{Model: } \text{Log10(Permeability)} = \text{Intercept} + \text{Slope} * \text{Porosity} + \text{Residual}$$

|                                         |                     |
|-----------------------------------------|---------------------|
| Degrees of freedom:                     | 152                 |
| Coefficient of determination:           | 0,164               |
| Standard error on the regression:       | 0,936 log(mD)       |
| Estimated intercept:                    | -1,722 log(mD)      |
| Estimated standard error of intercept : | 0,154 log (mD)      |
| Estimated slope:                        | 0,11319 log(mD) / % |
| Estimated standard error of slope:      | 0,02075 log(mD) / % |

Please note that the regression statistics pertain to log permeability values.

The coefficient of determination gives the fraction of the total variation squared which is explained by the mode. The standard error on the regression gives the mean 1 sigma error on the log permeability estimates.



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## 6. Appendix, data tabulation

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## 6.1 Laboratory analysis, GANE#1

General information on the analysis:

|                           |               |            |                     |
|---------------------------|---------------|------------|---------------------|
| Company:                  | GEUS          | Location:  | Greenland           |
| Depth interval:           | 487.28-636.86 | Core no. : | 156-204             |
| Depths are measured from: | KB            | Analysts:  | GG,HJL,MJ,LB,PET,GA |
| Depths are in:            | METRES        | Date:      | 301296              |
| Well:                     | GANE1         |            |                     |

**REMARKS :**

If "bublepermflow" are written as 0.0ml/300sec if less than 0.1ml/100s. I.e. 0 mD

Data not measured: “-”

The Geological Survey of Denmark and Greenland is fully responsible for the analytical results in the present report. The survey, however, bears no responsibility for decisions and interpretations based on the data presented.

| Sample<br>no. | Depth<br>m | Plug<br>type | Gas perm<br>mD | Porosity<br>% | Density<br>g/ccm |
|---------------|------------|--------------|----------------|---------------|------------------|
| 740           | 487,78     | Hor          | 21,2           | 5,42          | 2,690            |
| 741           | 488,78     | Hor          | 27,8           | 5,09          | 2,695            |
| 742           | 489,80     | Hor          | 16,1           | 5,79          | 2,640            |
| 743           | 491,03     | Hor          | 17,4           | 5,51          | 2,676            |
| 744           | 491,94     | Hor          | 4,71           | 5,25          | 2,774            |
| 745           | 492,94     | Hor          | 5,53           | 5,10          | 2,613            |
| 746           | 494,21     | Hor          | 2,96           | 3,10          | 2,711            |
| 747           | 495,21     | Hor          | 4,71           | 3,50          | 2,620            |
| 748           | 496,28     | Hor          | 0,042          | 0,44          | 2,677            |
| 749           | 500,67     | Hor          | 0,047          | 6,11          | 2,667            |
| 750           | 501,86     | Hor          | -              | 6,00          | 2,618            |
| 751           | 505,01     | Hor          | -              | 1,55          | 2,675            |
| 752           | 514,35     | Hor          | 0,104          | 6,96          | 2,672            |
| 753           | 515,15     | Hor          | 0,59           | 7,67          | 2,666            |
| 754           | 516,47     | Hor          | -              | -             | -                |
| 755           | 516,76     | Hor          | -              | 11,06         | 2,852            |
| 756           | 518,18     | Hor          | -              | 5,28          | 2,630            |
| 757           | 519,00     | Hor          | 0              | 0,70          | 2,669            |
| 758           | 519,78     | Hor          | 0              | 3,60          | 2,662            |
| 759           | 520,44     | Hor          | -              | 4,25          | 2,621            |
| 760           | 521,55     | Hor          | 6,03           | 2,71          | 2,574            |
| 761           | 522,60     | Hor          | 0,014          | 2,59          | 2,577            |
| 762           | 523,61     | Hor          | 0,005          | 1,82          | 2,698            |
| 763           | 524,76     | Hor          | 0,005          | 4,87          | 2,710            |
| 764           | 526,18     | Hor          | 0,005          | 3,03          | 2,699            |
| 765           | 527,18     | Hor          | 0,732          | 4,33          | 2,623            |
| 766           | 528,12     | Hor          | 0,008          | 5,55          | 2,660            |
| 767           | 529,12     | Hor          | 0,013          | 4,74          | 2,654            |
| 768           | 530,52     | Hor          | 0,015          | 5,71          | 2,692            |
| 769           | 530,70     | Hor          | 0,015          | 2,28          | 2,652            |
| 770           | 532,33     | Hor          | 0,728          | 1,80          | 2,588            |
| 771           | 532,88     | Hor          | 0,022          | 1,90          | 2,599            |
| 772           | 534,15     | Hor          | 0,004          | 1,32          | 2,669            |
| 773           | 535,27     | Hor          | 1,38           | 3,29          | 2,608            |
| 774           | 535,53     | Hor          | 0,006          | 0,46          | 2,691            |
| 775           | 538,81     | Hor          | 0,037          | 3,54          | 2,660            |
| 776           | 539,66     | Hor          | 2,2            | 2,22          | 2,606            |
| 777           | 540,06     | Hor          | 0,307          | 2,28          | 2,547            |
| 778           | 540,69     | Hor          | -              | 3,57          | 2,632            |
| 779           | 541,95     | Hor          | 0              | 0,43          | 2,689            |
| 780           | 542,88     | Hor          | 0,03           | 2,28          | 2,601            |
| 781           | 545,14     | Hor          | -              | 4,71          | 2,617            |
| 782           | 545,57     | Hor          | 4,47           | 3,65          | 2,622            |
| 783           | 546,74     | Hor          | 9,37           | 5,59          | 2,574            |
| 784           | 547,88     | Hor          | 0              | 3,23          | 2,678            |
| 785           | 548,72     | Hor          | -              | 3,51          | 2,631            |
| 786           | 549,78     | Hor          | 0,057          | 7,46          | 2,642            |
| 787           | 550,84     | Hor          | 0,026          | 8,98          | 2,645            |
| 788           | 552,13     | Hor          | 0,016          | 8,95          | 2,676            |

| Sample<br>no. | Depth<br>m | Plug<br>type | Gas perm<br>mD | Porosity<br>% | Density<br>g/ccm |
|---------------|------------|--------------|----------------|---------------|------------------|
| 789           | 556,16     | Hor          | 0,012          | 5,32          | 2,688            |
| 790           | 555,05     | Hor          | 0,03           | 6,43          | 2,662            |
| 791           | 556,19     | Hor          | 0,049          | 8,90          | 2,653            |
| 792           | 557,24     | Hor          | 0,059          | 6,76          | 2,646            |
| 793           | 558,53     | Hor          | 0,082          | 10,59         | 2,654            |
| 794           | 559,97     | Hor          | 0,214          | 12,57         | 2,648            |
| 795           | 560,58     | Hor          | 0,057          | 9,35          | 2,673            |
| 796           | 561,81     | Hor          | 0,016          | 7,40          | 2,675            |
| 797           | 562,75     | Hor          | 0,017          | 4,17          | 2,659            |
| 798           | 563,84     | Hor          | -              | 7,46          | 2,629            |
| 799           | 567,41     | Hor          | 0,009          | 2,18          | 2,693            |
| 800           | 566,93     | Hor          | 0,012          | 8,07          | 2,743            |
| 801           | 569,06     | Hor          | 0,01           | 2,41          | 2,691            |
| 802           | 570,00     | Hor          | 0,009          | 5,07          | 2,660            |
| 803           | 570,10     | Hor          | -              | 5,27          | 2,632            |
| 804           | 570,60     | Hor          | 0,009          | 4,28          | 2,687            |
| 805           | 570,98     | Hor          | 0,005          | 0,57          | 2,681            |
| 806           | 572,26     | Hor          | 0,986          | 9,78          | 2,644            |
| 807           | 572,73     | Hor          | 0,69           | 9,22          | 2,645            |
| 808           | 573,08     | Hor          | 2,24           | 5,77          | 2,629            |
| 809           | 574,88     | Hor          | 0,481          | 6,05          | 2,602            |
| 810           | 574,99     | Hor          | 0,393          | 3,70          | 2,614            |
| 811           | 576,60     | Hor          | 0,442          | 3,57          | 2,593            |
| 812           | 577,31     | Hor          | -              | 4,04          | 2,680            |
| 813           | 578,06     | Hor          | 0,002          | 0,91          | 2,670            |
| 814           | 578,70     | Hor          | 0,005          | 1,18          | 2,668            |
| 815           | 579,40     | Hor          | 0,004          | 4,48          | 2,652            |
| 816           | 580,47     | Hor          | 0,67           | 5,77          | 2,641            |
| 817           | 581,49     | Hor          | 0,059          | 1,67          | 2,679            |
| 818           | 594,28     | Hor          | 0              | 1,34          | 2,669            |
| 819           | 594,37     | Hor          | 0              | 1,59          | 2,662            |
| 820           | 595,99     | Hor          | 0              | 2,30          | 2,618            |
| 821           | 597,06     | Hor          | -              | 1,70          | 2,695            |
| 822           | 598,53     | Hor          | 1,22           | 6,37          | 2,857            |
| 823           | 598,94     | Hor          | 0              | 0,48          | 2,674            |
| 824           | 599,19     | Hor          | 0              | 0,43          | 2,688            |
| 825           | 599,79     | Hor          | 0,01           | 3,80          | 2,667            |
| 826           | 600,23     | Hor          | 0,007          | 3,73          | 2,666            |
| 827           | 600,33     | Hor          | 0,004          | 4,36          | 2,690            |
| 828           | 601,79     | Hor          | 0,004          | 3,29          | 2,670            |
| 829           | 602,69     | Hor          | 13,9           | 6,67          | 2,518            |
| 830           | 602,72     | Hor          | 0,009          | 5,29          | 2,649            |
| 831           | 603,58     | Hor          | 0,01           | 3,87          | 2,703            |
| 832           | 604,53     | Hor          | 0,015          | 5,03          | 2,644            |
| 833           | 604,77     | Hor          | 0,485          | 4,24          | 2,643            |
| 834           | 605,63     | Hor          | 1,8            | 4,72          | 2,559            |
| 835           | 607,21     | Hor          | 0,017          | 3,40          | 2,593            |
| 836           | 608,12     | Hor          | 0,012          | 4,73          | 2,628            |
| 837           | 608,13     | Hor          | 0,025          | 4,86          | 2,604            |
| 838           | 608,73     | Hor          | 0,036          | 5,91          | 2,654            |

| Sample<br>no. | Depth<br>m | Plug<br>type | Gas perm<br>mD | Porosity<br>% | Density<br>g/ccm |
|---------------|------------|--------------|----------------|---------------|------------------|
| 839           | 609,03     | Hor          | 0,056          | 9,68          | 2,718            |
| 840           | 609,23     | Hor          | 0,113          | 8,04          | 2,639            |
| 841           | 609,49     | Hor          | 0,038          | 7,08          | 2,678            |
| 842           | 610,73     | Hor          | 0,004          | 2,01          | 2,715            |
| 843           | 611,09     | Hor          | -              | 3,18          | 2,674            |
| 844           | 611,60     | Hor          | 0,021          | 4,41          | 2,632            |
| 845           | 612,85     | Hor          | 0,015          | 3,97          | 2,671            |
| 846           | 613,36     | Hor          | 0,008          | 2,25          | 2,680            |
| 847           | 613,96     | Hor          | 0              | 2,66          | 2,625            |
| 848           | 615,71     | Hor          | 0,355          | 12,26         | 2,655            |
| 849           | 616,02     | Hor          | 0,234          | 11,56         | 2,652            |
| 850           | 617,43     | Hor          | 0              | 2,88          | 2,606            |
| 851           | 618,27     | Hor          | 0,116          | 4,66          | 2,636            |
| 852           | 618,87     | Hor          | 0,138          | 10,03         | 2,644            |
| 853           | 619,55     | Hor          | 0,191          | 8,63          | 2,649            |
| 854           | 621,28     | Hor          | 0,194          | 12,27         | 2,654            |
| 855           | 621,80     | Hor          | 0,278          | 10,91         | 2,649            |
| 856           | 623,32     | Hor          | 0              | 3,18          | 2,694            |
| 857           | 623,78     | Hor          | 0,021          | 7,77          | 2,679            |
| 858           | 625,19     | Hor          | 0,033          | 4,15          | 2,626            |
| 859           | 626,82     | Hor          | 0              | 4,06          | 2,694            |
| 860           | 627,35     | Hor          | 0,07           | 5,76          | 2,659            |
| 861           | 627,75     | Hor          | 0,087          | 5,42          | 2,640            |
| 862           | 628,23     | Hor          | 0,053          | 5,15          | 2,633            |
| 863           | 628,73     | Hor          | 0,019          | 6,49          | 2,658            |
| 864           | 629,04     | Hor          | 0              | 4,79          | 2,743            |
| 865           | 629,44     | Hor          | 0,022          | 7,31          | 2,693            |
| 866           | 630,92     | Hor          | 0,076          | 11,10         | 2,663            |
| 867           | 631,36     | Hor          | 0,05           | 10,13         | 2,644            |
| 868           | 632,90     | Hor          | 0              | 3,15          | 2,629            |
| 869           | 635,22     | Hor          | 0,017          | 7,54          | 2,640            |
| 870           | 635,72     | Hor          | 0              | 1,39          | 2,596            |

## 6.2 Laboratory analysis , GANE#1A

General information on the analysis:

|                           |                 |            |                     |
|---------------------------|-----------------|------------|---------------------|
| Company:                  | GEUS            | Location:  | Greenland           |
| Depth interval:           | 636.02 - 706.68 | Core no. : | 206 - 258           |
| Depths are measured from: | KB              | Analysts:  | GG,HJL,MJ,LB,PET,GA |
| Depths are in:            | METRES          | Date:      | 301296              |
| Well:                     | GANE1A          |            |                     |

**REMARKS :**

If "boblepermflow" are written as 0.0ml/300sec if less than 0.1ml/100s. I.e. 0 mD

Data not measured: “-”

The Geological Survey of Denmark and Greenland is fully responsible for the analytical results in the present report. The survey, however, bears no responsibility for decisions and interpretations based on the data presented.

| Sample no. | Depth m | Plug type | Gas perm mD | Porosity % | Density g/ccm |
|------------|---------|-----------|-------------|------------|---------------|
| 871        | 633,23  | Hor       | 0,006       | 3,52       | 2,635         |
| 872        | 635,42  | Hor       | 0,006       | 5,40       | 2,663         |
| 873        | 363,15  | Hor       | 0           | 2,54       | 2,617         |
| 874        | 637,59  | Hor       | 0           | 2,62       | 2,656         |
| 875        | 644,11  | Hor       | 0,016       | 4,57       | 2,610         |
| 876        | 645,23  | Hor       | 0,44        | 6,12       | 2,611         |
| 877        | 646,36  | Hor       | 0,061       | 7,62       | 2,673         |
| 878        | 646,51  | Hor       | 0,015       | 6,38       | 2,669         |
| 879        | 646,78  | Hor       | 0,043       | 7,14       | 2,688         |
| 880        | 646,88  | Hor       | 35,1        | 6,56       | 2,715         |
| 881        | 647,27  | Hor       | 0,259       | 1,31       | 2,683         |
| 882        | 648,89  | Hor       | 0,007       | 3,87       | 2,623         |
| 883        | 649,48  | Hor       | 2,15        | 4,35       | 2,608         |
| 884        | 651,09  | Hor       | 0           | 1,23       | 2,662         |
| 885        | 651,29  | Hor       | 0,524       | 0,83       | 2,670         |
| 886        | 653,07  | Hor       | 0           | 1,14       | 2,649         |
| 887        | 654,41  | Hor       | 0           | 0,91       | 2,972         |
| 888        | 654,78  | Hor       | 0,005       | 2,60       | 2,695         |
| 889        | 656,79  | Hor       | 0,006       | 3,47       | 2,607         |
| 890        | 657,44  | Hor       | 0,01        | 4,07       | 2,616         |
| 891        | 358,09  | Hor       | 0,007       | 4,15       | 2,631         |
| 892        | 658,61  | Hor       | 0           | 0,65       | 2,792         |
| 893        | 659,17  | Hor       | 0,003       | 2,31       | 2,693         |
| 894        | 660,68  | Hor       | 0,007       | 5,36       | 2,612         |
| 895        | 661,25  | Hor       | 0,008       | 4,37       | 2,606         |
| 896        | 662,10  | Hor       | 0,126       | 5,20       | 2,650         |
| 897        | 663,51  | Hor       | 0,103       | 9,48       | 2,674         |
| 898        | 664,81  | Hor       | 9,08        | 16,76      | 2,650         |
| 899        | 665,44  | Hor       | 2,47        | 15,13      | 2,649         |
| 900        | 666,58  | Hor       | 1,81        | 14,33      | 2,850         |
| 901        | 667,43  | Hor       | 2,69        | 15,08      | 2,652         |
| 902        | 669,31  | Hor       | 0,681       | 10,60      | 2,654         |
| 903        | 670,37  | Hor       | 0,223       | 11,00      | 2,679         |
| 904        | 671,48  | Hor       | 2,91        | 15,52      | 2,656         |
| 905        | 672,17  | Hor       | 1,37        | 15,65      | 2,647         |
| 906        | 673,05  | Hor       | 1,6         | 14,97      | 2,653         |
| 907        | 674,46  | Hor       | 0,763       | 13,58      | 2,656         |
| 908        | 675,68  | Hor       | 0,817       | 13,11      | 2,654         |
| 909        | 676,75  | Hor       | 0,071       | 6,43       | 2,650         |
| 910        | 677,71  | Hor       | 1,27        | 13,57      | 2,656         |
| 911        | 678,63  | Hor       | 0,273       | 12,21      | 2,659         |
| 912        | 679,86  | Hor       | -           | 12,11      | 2,540         |
| 913        | 680,78  | Hor       | -           | 20,55      | 2,594         |
| 914        | 681,62  | Hor       | 0,8         | 11,71      | 2,608         |
| 915        | 682,26  | Hor       | 0,054       | 6,83       | 2,659         |
| 916        | 683,74  | Hor       | 0,036       | 8,75       | 2,660         |
| 917        | 684,26  | Hor       | 0,134       | 8,95       | 2,656         |
| 918        | 685,03  | Hor       | 0,133       | 10,05      | 2,655         |
| 919        | 686,00  | Hor       | 0,154       | 10,02      | 2,649         |

| Sample<br>no. | Depth<br>m | Plug<br>type | Gas perm<br>mD | Porosity<br>% | Density<br>g/ccm |
|---------------|------------|--------------|----------------|---------------|------------------|
| 920           | 687,11     | Hor          | 0,266          | 11,81         | 2,648            |
| 921           | 688,07     | Hor          | 0,062          | 9,54          | 2,648            |
| 922           | 688,96     | Hor          | 0              | 0,28          | 2,995            |
| 923           | 690,90     | Hor          | 0              | 0,15          | 2,989            |
| 924           | 691,84     | Hor          | 0              | 0,23          | 3,066            |
| 925           | 693,18     | Hor          | -              | 12,27         | 2,691            |
| 926           | 694,34     | Hor          | 0              | 0,53          | 3,056            |
| 927           | 695,23     | Hor          | 0              | 0,24          | 3,111            |
| 928           | 696,59     | Hor          | 0,048          | 9,35          | 2,655            |
| 929           | 697,41     | Hor          | 0,034          | 7,61          | 2,651            |
| 930           | 698,46     | Hor          | 0,101          | 7,24          | 2,656            |
| 931           | 699,29     | Hor          | 0,353          | 8,32          | 2,650            |
| 932           | 700,62     | Hor          | 1,06           | 10,25         | 2,638            |
| 933           | 701,86     | Hor          | 0,094          | 5,73          | 2,653            |
| 934           | 702,60     | Hor          | 0,328          | 9,82          | 2,644            |
| 935           | 703,71     | Hor          | 0,143          | 6,30          | 2,672            |
| 936           | 704,92     | Hor          | 0,635          | 9,43          | 2,647            |
| 937           | 706,20     | Hor          | 2,54           | 10,93         | 2,642            |